The Influence of the Surface Roughness of Aqueous Coated Samples and the Particle Size of the Coatings on the Reflection and Colourimetric Values of Offset Printed Samples

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The visual appearance of the final printed sheet is one of the upmost important characteristics of printed product, especially in the packaging market. Value added printing with a large number of surface and visual enhancement elements is improving the visual appeal and improving the optical properties of the objects. Coating is one of the most often used process not just to protect the printed sheet and speed up drying, but can be very useful in creating interesting visual effects on the surface of the printed substrate. The reflection, which is influenced by the properties of the surface texture and surface materials, can greatly change the final overall appearance. This change can be observed by the observer or recorded in values calculated by the colour or gloss measurement instruments. These changes can cause problems with colour proofing and colour prediction issues that are very important in the packaging industry. The topic of this paper is the investigation of the surface properties of agueous coated offset prints and the particle sizes of the used coatings. The surfaces were analysed with AFM microscope and the appropriate ISO surface roughness values were determined from the digital data of the scanned areas. The measurement of the particle sizes were done to determine the distribution volume, length of coatings particle sizes because the coating physical and chemical properties can influence the levelling of the coating on the surface and thus influence the forming of the final layer of the print surface. The influence of these factors on the reflection was determined by spectrophotometric measurement of the reflection and the appropriate colorimetric values. We have used two different type of aqueous (matte and glossy), which were applied with two different anilox rollers (60L/cm and 90L/cm), which were applied over conventional offset printing inks. The results show there is a correlation between the coating amount, surface levelling, particle distribution and the calculated colorimetric values.

1. Introduction

The process of added value printing involves several additional operations besides the basic printing of the ink on the carrying substrate. Additional liquid or solid materials are applied to the original printed surface to enhance the print surface. The change in the reflection is the observed as different light distribution from the changed surface. The most commonly applied liquid materials are coatings that usually come in form of oil-based varnishes, aqueous coatings and UV coatings. All of the materials have different physical and chemical properties and are applied through different mechanisms (roller based system, anilox chambered doctor blade system). Different drying processes beside aforementioned factors will also have influence on the final surface topography. Surface structure and the type of incoming light are one of the most influential parts of the light scattering effect and greatly influence the final printed product appearance. Consistent colour reproduction and accurate colour prediction is nowadays an essential part of the contemporary print production. Changes in appearances due to different types and quantities of coatings applied to the printed surface can cause problems in colour communication. Investigating the changes which certain coating properties like applied quantity and particle size distribution of the applied coating exert in correlation with the final texture of the coated surface after drying can gives us important process information's. This information can be used in process optimization, colour prediction and proofing and in environmental protection because of the optimized and controlled application of the coatings.

2. Statement of the problem

Varnishes (coatings) are applied directly to the substrate by rollers or coating forms in coating units or indirectly via intermediate carriers (e.g. print varnish from the printing plate via the blanket on the paper). Roller and blade systems (usually chambered doctor blades in conjunction with anilox rollers) are used to meter the quantity applied. [1] If the layer of the surface enhancing material is intended to be the functional layer or a protective layer it should be continues and without any damages. One of the prerequisites for forming such a layer is that the coating material is in liquid form at the moment of the application. One of the principal reasons is that the discrete particles of the coatings that are applied as separate drops should join to form a continous layer on the surface. Principal characteristic of these materials is the flow characteristics of these materials [2]. The flow and the surface levelling are a predicted movement of the coating materials before and after the application on the surface and these processes influence greatly the appearance of the coated surface [3]. The determination of the flow and the formation of the coating materials are influenced by number of factors, which are primarily connected with inter surface processes. Most of the coating materials have a relative low surface tension and are applied to the surfaces with higher surface tension that leads to the decrease of the total free surface energy. The process of the layer forming in the dispersion coating materials like the aqueous coatings and varnishes is the process of the joining of the polymer particles after the evaporation of the water from the emulsion system. This process enables the connection between the neighbouring polymer particles. Besides the forming of the coating layers surface texture, according to the corpuscular reflection theory which forms a bridge between the Kubelka-Munk coefficients and optical constants of particles the particles play significant role in light scattering. The development of this is centred on the theory of Mie, which links the physical constants, including particle size, with scattering and absorption properties of the particle [4]. The particle size distribution comes from the statistical analysis of the particle sizes in an ensemble (population). The distribution of the particle size parameter can be described in terms of particle size distribution curve. One of the most effective ways to plot these values is through the distribution density function. Finer particle size will yield better quality transparency and gloss due in part to film smoothness. In many coatings, especially industrial coatings, a variety of waxes, polyethylenes and other special hard polymers are used to impart certain properties to the cured film. Since these materials function by coming to the surface of the cured film, much of their beneficial and adverse effects are dependent on particle size. Since the action of these particles is at the surface of the film, it is obvious that the larger the particle, the greater the effect on film uniformity. Naturally, the larger the particle, the larger the crater and it results in a rougher, less uniform surface. This affects film integrity, transparency and gloss in clear coatings, as well as reflected image in pigmented coatings [5]. Almost all of the surfaces that are treated by some production process are far from an ideal smooth surface and contain more or less some measure of roughness. The properties of the surface texture are defined by the distribution, shape and the size of the elementary particles in the forms of peaks or valleys compared to the average "ideal" surface. In his PhD thesis [6] has stated a number of experimental data and theories about the influence of the surface roughness on the light scattering and thus defined to the importance of

defining this property in the evaluation of the light. The methods for surface texture and roughness evaluation can be generally classified as contact and non-contact methods, as well as three dimensional (surface) or two dimensional (profiles) methods [7]. For any given rough surface, it is possible to measure its surface profile with a light beam or a mechanical stylus. In principle, from these surface profile measurements we can calculate the surface scattering. However, all profile measurements are limited by the instruments' bandwidth. Even if we know the exact surface profile, we still have to know the precise location of the light beam relative to the surface before we can calculate the exact light scattering numerically. Practically, for almost all applications, we are only interested in the statistical properties of the roughness and their effect on light scattering [8]. Atomic Force Microscopy (AFM) is a contemporary 3D scanning methodology which can calculated these statistical properties from a scanned surface and by using additional software we can generate appropriate 3D data of the surface. The values obtained can be described by numerical numbers and can be used to control the changing of the surface properties and thus by measuring additional values as gloss and colour values the influence of the surface roughness on the colorimetric values. Surface roughness is mostly associated with interface reflection and less by body reflection, which is governed by the subsurface material. Several papers deal with different roughness correlated reflection values on gloss coated samples as in [9], digital printed samples [10] and the influence of the varnish on the colour values of the prints in [11]. The later papers found that the varnish (coating) layer doesn't affect so much the hue, but the saturation and lightness of the samples. In an another paper by [12] goniocolorimetric measurements of coated samples were made and the authors found that lightness, chroma, and hue angle in the gloss angle region suffer as a result of high changes and extremes depending on the gloss of the material tested. This is what complicates color measurements and full determination or definition of the complex appearance of printed materials. The change of Chroma with varnishing of glossless materials was clearly elucidated. The colorimetric measurement of these values can yield (change?) considerably depending on the instrument type and measurement geometry [13] so there are few more problems to be solved in the future regarding the quality control of coated samples.

3. Experimental

Methods and materials In the experimental part we have printed the prints with conventional offset inks which confirm to the ISO 2864 standard and the inking was done according to the ISO 12647-2:2004 on the glossy coated paper of 130g/m^2 which conforms to a Type 1 paper of the same standard. For the coating we have used an inline anilox roller coating system with two different anilox rollers of 60L/cm and 90L/cm to regulate different amounts of the applied aqueous coating. We have used two commercial coatings the glossy Prestofix Hochglanzlack H6055/55 and the matte Prestofix Mattlack H260/55 aqueous coating. The drying and the coating were handled on the basis of the offset press and coating supplier recommendations. After the prints were dried and the final coating layer was formed we have selected the sheets by random sampling method from the OK prints. The presented results are the averaged values of these prints. The liquid coating was tested in regards to its the particle distribution in the laboratory with a Malvern Mastersizer 2000 Particle Size Analyzer. It is capable of analyzing particles between 0.02 and 2000 µm. The Malvern Mastersizer 2000 records the light pattern scattered from a field of particles at different angles. An analytical procedure is then used to determine the size distribution of spherically shaped particles that created the patterns. The result of the analysis is the relative distribution of volume (number) of particles in the range of size classes. Measurement parameters were: pump speed 2500 rpm: ultrasonic. off.

For the surface roughness analysis we have used the Veeco CP-II AFM microscope where we have scanned 6 positions on the non coated and coated samples in x and y direction, and from the sample sizes of 80 x 80 μ m² the statistical ISO roughness values were determined and averaged. The ISO roughness values and the 3D data were generated by Gwyddion and Image Metrology SPIP software packages. All the samples before the analysis were corrected with mean plane subtractions. The colorimetric data and the reflectance curves were measured with Techkon SpectroDens reflective spectrophotometer. We have used the 0/45° directional measurement geometry, with D₅₀ standard illuminant and 2^o standard observer. The relative reflectance was sampled between 400 and 700 nm, and from these data were also the CIE D₉₄ color differences calculated.

4. Results

The analyses of the glossy and matte sample particle sizes were done by volume, number and length distributions. The distribution curve of the volume analysis of the glossy coating is presented in Figure 1 and matte coating in Figure 2.









As we can observe from Figure 1 in the glossy coating there is a high volume ratio around a particle size of 100 μ m while for the matte coating there is a larger volume ration for the particles between 1 and 10 μ m and a smaller volume of particles with sizes around 100 μ m. In the analysis of the number of the particles we can see in Figure 3 that for the glossy coating the largest number of particles are between 0.1 and 0.5 μ m. In Figure 4 the number of particles of matte coating shows that there is larger number of particles in the region from 0.9 to 9 μm . This shows that the matte coating has large particles than the glossy coating.



Figure 4: Particle size distribution of matte aqueous coating in terms of number

After the coating particle distribution we have evaluated the surface roughness values from the scanned areas of the samples. For the quantification of the surface roughness we have chosen the average surface roughness factor Sa that conforms the ISO/DIS 25178-2 and ASME B46.1 standards and recommendations and is calculated with the following expression:

$$S_{a} = \frac{1}{MN} \frac{M-1}{\sum_{k=0}^{N-1} \sum_{l=0}^{N-1} |z(x_{k}, y_{l})|$$
(1)

where M is the number of points per profile, and N is the number of profiles within the sampling area.

The results of surface roughness evaluation of the non-coated printed and coated samples are presented in Figure 5.

As we can see from the results in Figure 5 the average surface roughness of plain paper and printed paper is guite similar (99.11 and 100.52 nm) while with the application of glossy coating the surface roughness is lower. The higher coating amount transferred with the 60L/cm anilox roller yielded 3.96 g/m² coating amount and surface roughness of 47.93 nm which was the lowest of all samples, while the finer 90L/cm anilox transferred 1.9 g/m² and had a slightly rougher surface of 66.41 nm which was lower from all samples expect the glossy coated samples with higher amount. The application of the matte coating in a smaller amount (90L/cm roller) resulted in value of 1.13 g/m² and rougher surface of 229.42 nm, while a higher amount of transferred matte coating (60L/cm roller) 2.15 g/m² and the roughest surface of 244.07 nm. We can observe that with higher amount of glossy coating there is a decrease in surface roughness and with higher amount of matte coating there is an increase of average surface roughness of the prints.



Figure 5: The averaged Sa surface roughness values of the measured samples To gain a more accessible knowledge of the encountered surface roughness properties we have generated a 3D representation of the surfaces. The Figures 6a to f repre-

sents the typical topography of the observed and measured samples.



Figure 6: The surface topography of a) glossy coated paper no ink no coating b) printing ink with no coating c) glossy coating applied with 90L/cm anilox roller d) glossy coating applied with 60L/cm anilox roller e) matte coating applied with 90L/cm anilox roller f) matte coating applied with 60L/cm anilox roller e) matte coating applied with 90L/cm anilox roller f) matte coating applied with 60L/cm anilox roller f) matter coating applied with 6

As a final measurement we have measured the reflectance spectra and colour differences of the non coated and coated samples. We have measured the values on the full tone (100% tone value) CMYK patches. The results of the colour difference values measurement for the glossy coated samples are presented in Figure 7. The reflection spectra of the black colour patch from the coated and non-coated samples is presented in Figure 8. The values for Δa , Δb and ΔL of the coated samples are shown in Table 1.



Figure 7: Colour difference values of different coated CMYK patches

Anilox roller (90	L/cm)	ΔL	∆a	Δb	ΔE	ΔE94	σ (ΔΕ)
Cyan		0.54	-0.99	1.24	1.68	0.96	0.09
Magenta		-0.86	1.84	1.75	2.68	1.29	0.23
Yellow		0.29	0.11	2.87	2.89	0.63	0.2
Black		-5.92	1.19	3.06	6.77	6.58	0.31
Anilox roller (60	L/cm)	ΔL	∆a	Δb	ΔE	ΔE94	σ (ΔΕ)
Cyan		-1	-1.22	0.8	1.77	1.25	0.07
Magenta		-0.59	1.78	2.3	2.96	1.32	0.12
Yellow		0.24	0.22	3.49	3.5	0.72	0.32
Black		-5.6	1.29	3.44	6.7	6.46	0.20



As we can observe from Figure 7 there is a very small but measurable colour difference with the additional amount of glossy coating where the higher amount usually results in a higher colour difference value. The most prominent change is the black colour patch that has the most noticeable visual difference off all samples. All the colour samples have larger differences in the chromatic part (Δa , Δb) then in the lightness value (Δl) except for the black where the largest difference is in the lightness component of the stimulus. This leads in colour appearance to darker more saturated samples in the coated samples. To verify this throughout the visible spectrum we made the measurements of the reflection curves on the patches and the result for the black sample is presented in Figure 8. We can observe that both coated samples have a smaller reflection throughout the measured range then the uncoated sample. The larger applied coating quantity gave slightly lower reflection values, which can be due to smoother surface, which reflects more in the specular region and thus reflects less to the measurement device sensor, which is recorded as darker lower reflection value. The results for the matte coatings are presented in Figure 9 and Figure 10 and Table 2.



Figure 9: Colour difference values of different coated CMYK patches

Anilox roller (90L/cm)	ΔL	Δa	Δb	ΔE	ΔE94	σ (ΔΕ)
Cyan	2.29	2.06	2.43	3.93	2.45	0.13
Magenta	2.64	-3.5	0.92	4.48	2.8	0.17
Yellow	1.11	-0.11	-6.09	6.19	1.61	0.2
Black	4.91	-1.28	-2.45	5.63	5.48	0.26
Anilox roller (60L/cm)	ΔL	Δa	Δb	ΔE	ΔΕ94	σ (ΔΕ)
Cyan	2.43	2.71	2.11	4.2	2.63	0.12
Magenta	3.38	-4.68	0.62	5.8	3.56	0.36
Yellow	1.27	-0.65	-8.64	8.76	2.12	0.17
Black	6.32	-1.15	-2.29	6.81	6.7	0.31

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From Figure 9 and 10 we can see that as well with the glossy samples, the higher amount of matte coating resulted in higher colour difference values from the printed but not coated offset samples. The colour difference ranges from 1.61 to 5.68 for the 90L/cm anilox roller to 2.12 to 6.7 for the 60L/cm anilox roller. It can be observed that the differences are somewhat higher, and

again the black colour patch yielded the highest difference values. The relative reflection curves of the samples show that the matte coating gives a slightly higher reflection and thus producing a lighter sample. The higher the amount of the applied coating the lighter and less saturated seems the colour patch. These differences are also influenced by the measurement geometry of the used instrument where more information is distributed in the diffuse angles and thus giving more light to the colour sensor. These changes are far more recorded then the changes in lightness except for the black colour which of course has low chromacity values. These measured values correspond well with the visual observations of the printed and coated samples, which are prone to colour change due to textured surface viewing angle.

5. Conclusion

On the basis of results found in the study we can observe a few different effects. By analyzing particles in the aqueous coating we have found differences between the density distribution of the coating particles in volume and dominant sizes. In the number distribution we found that the glossy coating has a large ratio of small particle sizes. while the matte coating has a larger ratio of somewhat larger sized particle especially in the 0.9 to 10 µm particle size region. The AFM scanning of the surface showed numerical differences as well very visible differences on the 3D visualized data. The surface roughness of the initial printed but not coated samples are being smoothened with every additional amount of glossy coating that is showed by the decrease of average surface roughness. The matte coating increases the average surface roughness parameter, which is also very noticeable on the 3D data of the scanned surface that exerts a very rough surface with large offset of valley and heights. The colorimetric data shows a increase which is small in terms of visual approximation for the cyan, magenta, yellow while the black yielded the largest differences for the glossy coatings and even larger instrumental and visual differences for the matte coating. These differences are also noticeable in the reflection curve of all colour samples. The results of this study can be used to improve the predictability of coating production process, and provide and insight in the levelling and forming of the coating layer. From this experimental data further information can be extracted which can provide colorimetric data for soft and hard proofing of the coated samples. Finding the appropriate colour change correlation in terms of coating type and quantity would be useful in construction of appropriate colour prediction tool for prepress. The soft proof software tool could be constructed with and option of coating type and guantity selection and additional colour change algorithms could be implemented in already available proofing solutions. The ability of predicting colour changes in terms of the applied coating quantity would lead to

better process control, easier production and also environmental benefits which all lead to safer and efficient print production.

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6. References

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